



4C grading

1. Description

SR TIMSORT (call in simulation_4C if flag_wpm=1) generates a list of assortments of the available timber. timsort.f is called per year, generating the list of 'timber pieces' of the whole stand separated for the remaining and harvested part of the stand. The output of the assortments with information about the diameter, lenght, volume and species is given in an output data file <name>_mansort.out* (harvested part) und <name>_standsort.out* (remaining part).

Following information are used

- a data set for grading per species with data about minimum lenght, minimum diameter (see Table 1)
- data about bark (see Table 2, data field rabz in amod_tisort.f)

Per tree cohort the following variables are used:

N (number), H (height), HBO (bole height), DBH, DCRB (trunk diameter at crown base)

The grading uses 6 categories according to Table 1, called STE, SG1, SG2, IN1, IN2, FUE (see Table 3).

Grading is controlled by flag_sort

Flag_sort = 0 : all assortments

Flag_sort = 1 : no STE, all other

Flag_sort = 2 : only SG2 (3m), IN1,IN2, FUE

Flag_sort = 3 : only SG1 (4m), IN1,IN2, FUE

2. Calculation of required variables

suml - length of the always measured stem segments

Dborg – basis diameter at height stoh (stump height)

Horg – height of the total stem

Dbase – diameter at the stem base

a) Diameter Db at height Hs = STOH (STOH = 10 cm)

if HBO = 0.:

$$Dborg = \frac{(Horg - STOH) * Dbase}{Horg}$$

else

$$Dborg = DCRB + (Dbase - DCRB) * \frac{(HBO - STOH)}{HBO}$$

b) Diameter Dx at height Hx:

$Hx \leq HBO$

$$\tan \alpha = \frac{Dborg - DCRB}{HBO} = \frac{Dx - DCRB}{(HBO - suml - Hx)}$$

$$Dx = \frac{(Dborg - DCRB)(HBO - suml - Hx)}{HBO} + DCRB$$

$Hx > HBO$

$$\tan \beta = \frac{DCRB}{2(Horg - HBO)} = \frac{Dx}{2(Horg - suml - Hx)}$$

$$Dx = \frac{DCRB(Horg - suml - Hx)}{(Horg - HBO)}$$

DCRB=0

$$Dx = Dborg \frac{Horg - suml - Hx}{(Horg - stoh)}$$

c) height Hx at diameter Dx

DCRB < Dx

$$\frac{HBO}{Dborg - DCRB} = \frac{HBO - suml - Hx}{Dx - DCRB}$$

$$Hx = HBO - suml - \frac{HBO(Dx - DCRB)}{Dborg - DCRB}$$

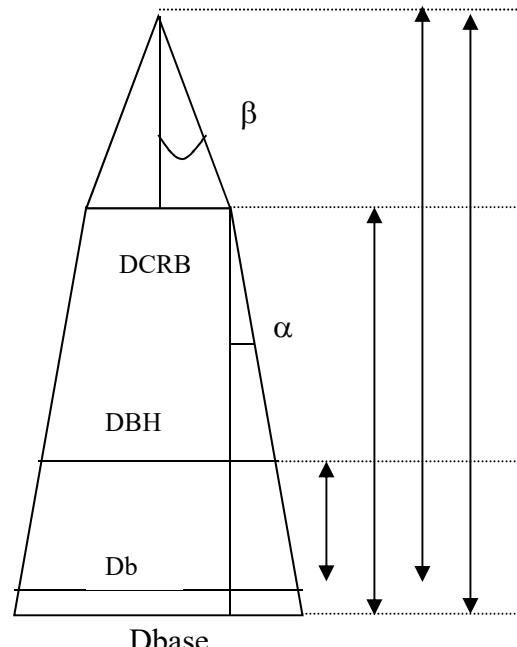


Figure 1 stem variables



DCRB > Dx

$$\frac{H_{org} - HBO}{DCRB} = \frac{H_{org} - H_x - suml}{dx}$$

$$H_x = H_{org} - suml - \frac{(H_{org} - HBO)Dx}{DCRB}$$

DCRB = 0

$$H_x = H_{org} - suml - \frac{(H_{org} - stoh)Dx}{Db_{org}}$$

3. Variables for grading

For data and definitions see Table 1:

RABZ – bark extraction (Table 2)

LMIN - minimum diameter at H=0.1 m

LDMIN - minimum diameter at Hlzmin/2

LZMIN

LASFIXL1

LASFIXL2

LASDMIN

LASZMIN

ZUS addition at stem length (5cm, 10 cm,)

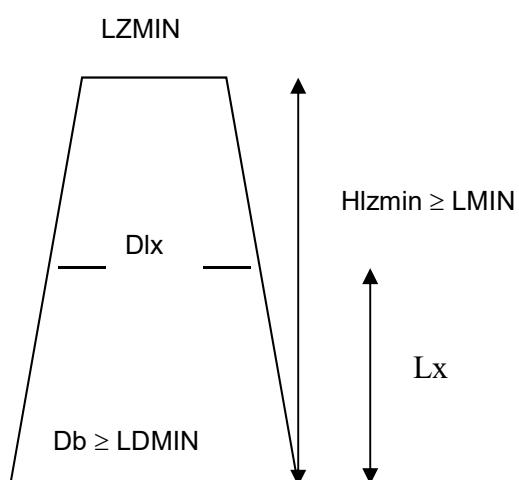


Figure 2 stem section characteristics

Per species

Per diameter class, per cohort

$Db \leq LZMIN$ yes \longrightarrow fulewood



no
Hlzmin is calculated: stem length Hx with Dx= LZMIN

Hlzmin \leq LMIN yes —————> industrial wood
↓ no
Lx = Hzmin/2

Dlx is calculated: diameter at height Lx

Dlx \leq LDMIN yes —————> stem sections
↓ no
calculation of the volume of the stem

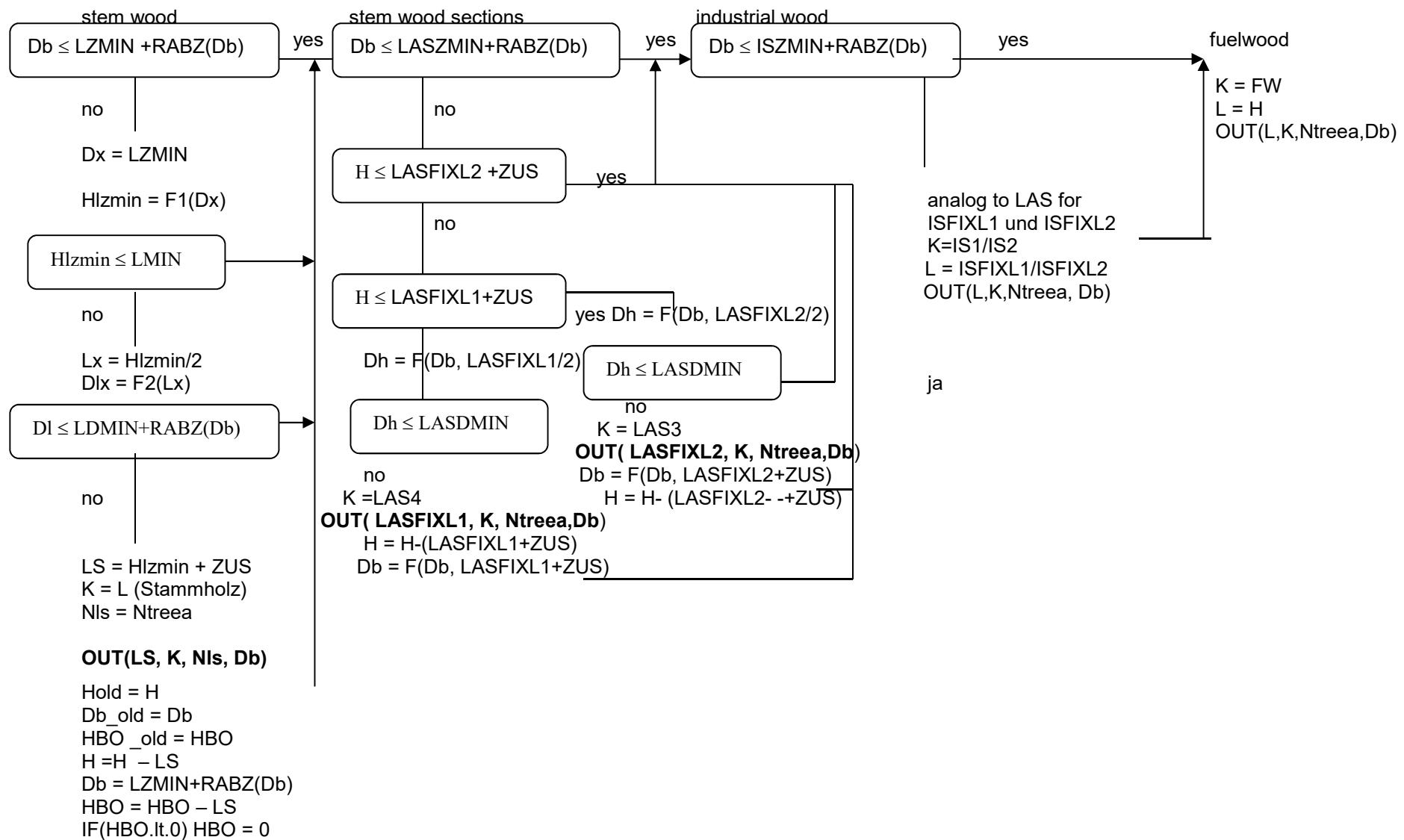


Figure 3 Flow Diagram of grading

Table 1 Parameter for timber grading in 4C (P. Mohr)

| Species group | species | Stump height [m] | Stem wood (L) – min. lengtht [m] | L-min. diameter [cm o.R.] | L-min. top diameter [cm o.R.] | Wood section (LAS) - length 1 [m] | LAS -length 2 [m] | LAS-min. diameter [cm o.R.] | LAS –min. top diameter [cm o.R.] | Ind. wood(IS)-length 1 [m] | IS-length 2 [m] | IS-min. diameter [cm o.R.] | IS-min. top diameter [cm m.R.] | Fuel wood (BRH) |
|--------------------------------|---------------------|------------------|----------------------------------|---------------------------|-------------------------------|-----------------------------------|-------------------|-----------------------------|----------------------------------|----------------------------|-----------------|----------------------------|--------------------------------|-----------------|
| BAGRP | BAUM | STOH | LMIN | LDMIN | LZMIN | LASFIXL1 | LASFIXL2 | LASADMIN | LASZMIN | ISFIXL1 | ISFIXL2 | ISDMIN | ISZMIN | BRH |
| Pinelike needle wood Nadelholz | Pine larch | 0.1 | 4 | 30 | 14 | 4 | 3 | 15 | 11 | 2 | 1 | 10 | 7 | |
| Sprucelike needle wood | Spruce, Douglas fir | 0.1 | 4 | 30 | 14 | 4 | 3 | 15 | 11 | 2 | 1 | 10 | 7 | |
| Soft broadleaved. wood | birch | 0.1 | 4 | 35 | 20 | 4 | 3 | 20 | 11 | 2 | 1 | 10 | 7 | |
| Hard broadleaved wood | Beech, oak | 0.1 | 4 | 30 | 20 | 4 | 3 | 20 | 11/ 18 (Bäucker) | 2 | 1 | 10 | 7 | |

o.R. – without bark

Table 2 bark extraction DM- diameter in the middle of the stem (section)

| Species | DM [cm] | Bark [cm] |
|---------|---------|-----------|
| beech | < 35 | 1 |
| | >35 | 2 |
| spruce | < 25 | 1 |
| | 25-40 | 2 |
| | > 40 | 3 |
| pine | < 20 | 1 |
| | 20-30 | 2 |
| | > 30 | 4 |
| oak | < 40 | 3 |
| | 40-60 | 5 |
| | > 60 | 6 |
| birch | < 40 | 2 |

New assortment for pine LAS1a (Juli 2003): with LAS1DMIN = 11 and LAS1ZMIN = 11; length as for LAS

Table 3 timber assortment abbreviations

| Model 4C | Timber grade | |
|-----------------|---------------------|----------------------------|
| ste | L | Stem wood |
| sg1 | LAS 1 | wood sections length 1 |
| sg2 | LAS2 | wood sections length 2 |
| in1 | IS1 | industrial timber length 1 |
| in2 | IS2 | industrial timber length 1 |
| fue | BRH | Fuel wood |

Example of output in file <name>_standsort.out

diam_wob : diameter without bark

t_d_wob: top diameter without bark

top_d – diameter at top

Sortiment of whole stand (without harvested trees)

| year | count | spec | type | cm len | cm diam | cm diam_wob | cm top_d | cm t_d_wob | M³/ha Volume | Kg C/ha DW | number |
|------|-------|------|------|-----------|------------|----------------|-------------|---------------|-----------------|---------------|--------|
| 1 | 326 | 4 | fue | 354.229 | 4.317 | 1.317 | 0 | 0 | 0.0022 | 0.621 | 14 |
| 1 | 325 | 4 | fue | 625.218 | 5.587 | 2.587 | 0 | 0 | 0.0058 | 1.614 | 24 |
| 1 | 324 | 4 | fue | 870.851 | 8.157 | 5.157 | 0 | 0 | 0.0146 | 4.08 | 35 |
| 1 | 323 | 4 | fue | 1146.379 | 10.065 | 7.065 | 0 | 0 | 0.0327 | 9.162 | 17 |
| 1 | 322 | 4 | fue | 1344 | 11.808 | 8.808 | 0 | 0 | 0.0581 | 16.262 | 5 |
| 1 | 321 | 4 | fue | 1367 | 12.665 | 9.665 | 0 | 0 | 0.0697 | 19.52 | 3 |
| 1 | 320 | 4 | in1 | 210 | 13.255 | 10.255 | 12.665 | 9.665 | 0.0291 | 8.156 | 3 |
| 1 | 319 | 4 | fue | 826.194 | 12.667 | 9.667 | 0 | 0 | 0.0347 | 9.717 | 1 |
| 1 | 318 | 4 | in1 | 210 | 14.014 | 11.014 | 12.667 | 9.667 | 0.0311 | 8.701 | 1 |
| 1 | 317 | 4 | in1 | 210 | 15.436 | 12.436 | 14.759 | 11.759 | 0.0395 | 11.06 | 1 |
| 1 | 316 | 4 | fue | 920 | 12.963 | 9.963 | 0 | 0 | 0.0405 | 11.332 | 2 |
| 1 | 315 | 4 | in1 | 210 | 14.356 | 11.356 | 12.963 | 9.963 | 0.0328 | 9.179 | 2 |
| 1 | 314 | 4 | in1 | 210 | 15.792 | 12.792 | 15.204 | 12.204 | 0.0413 | 11.566 | 2 |
| 1 | 313 | 4 | in1 | 210 | 17.026 | 14.026 | 16.439 | 13.439 | 0.048 | 13.44 | 2 |
| 1 | 312 | 4 | in1 | 210 | 18.261 | 15.261 | 17.673 | 14.673 | 0.0552 | 15.455 | 2 |
| 1 | 311 | 4 | in1 | 210 | 19.495 | 16.495 | 18.907 | 15.907 | 0.0629 | 17.61 | 2 |
| 1 | 310 | 4 | fue | 950 | 14.679 | 11.679 | 0 | 0 | 0.0536 | 15.006 | 5 |
| 1 | 309 | 4 | in1 | 210 | 15.787 | 12.787 | 14.679 | 11.679 | 0.04 | 11.209 | 5 |
| 1 | 308 | 4 | in1 | 210 | 17.076 | 14.076 | 16.462 | 13.462 | 0.0483 | 13.521 | 5 |
| 1 | 307 | 4 | in1 | 210 | 18.365 | 15.365 | 17.751 | 14.751 | 0.0558 | 15.634 | 5 |
| 1 | 306 | 4 | in1 | 210 | 19.654 | 16.654 | 19.04 | 16.04 | 0.0639 | 17.901 | 5 |
| 1 | 305 | 4 | in1 | 210 | 20.943 | 17.943 | 20.329 | 17.329 | 0.0726 | 20.321 | 5 |
| 1 | 304 | 4 | fue | 878 | 14.434 | 11.434 | 0 | 0 | 0.0479 | 13.409 | 4 |
| 1 | 303 | 4 | in1 | 210 | 16.06 | 13.06 | 14.434 | 11.434 | 0.0431 | 12.077 | 4 |
| 1 | 302 | 4 | in1 | 210 | 18.658 | 15.658 | 17.848 | 14.848 | 0.0569 | 15.938 | 4 |
| 1 | 301 | 4 | in1 | 210 | 19.878 | 16.878 | 19.297 | 16.297 | 0.0654 | 18.307 | 4 |
| 1 | 300 | 4 | in1 | 210 | 21.098 | 18.098 | 20.517 | 17.517 | 0.0736 | 20.618 | 4 |
| 1 | 299 | 4 | in1 | 210 | 22.317 | 19.317 | 21.736 | 18.736 | 0.0824 | 23.066 | 4 |

| | | | | | | | | | | | |
|---|-----|---|-----|-----|--------|--------|--------|--------|--------|--------|---|
| 1 | 298 | 4 | in1 | 210 | 23.537 | 20.537 | 22.956 | 19.956 | 0.0916 | 25.652 | 4 |
| 1 | 297 | 4 | fue | 675 | 11.967 | 8.967 | 0 | 0 | 0.0253 | 7.086 | 4 |
| 1 | 296 | 4 | in1 | 210 | 13.714 | 10.714 | 11.967 | 8.967 | 0.0316 | 8.849 | 4 |
| 1 | 295 | 4 | in1 | 210 | 17.383 | 14.383 | 15.636 | 12.636 | 0.0505 | 14.147 | 4 |
| 1 | 294 | 4 | in1 | 210 | 20.547 | 17.547 | 19.305 | 16.305 | 0.0676 | 18.933 | 4 |
| 1 | 293 | 4 | in1 | 210 | 21.749 | 18.749 | 21.177 | 18.177 | 0.0782 | 21.908 | 4 |
| 1 | 292 | 4 | in1 | 210 | 22.951 | 19.951 | 22.379 | 19.379 | 0.0871 | 24.392 | 4 |
| 1 | 291 | 4 | sg1 | 410 | 24.725 | 21.725 | 23.581 | 20.581 | 0.1975 | 55.29 | 4 |
| 1 | 290 | 4 | fue | 754 | 14.321 | 11.321 | 0 | 0 | 0.0405 | 11.335 | 7 |
| 1 | 289 | 4 | in1 | 210 | 16.195 | 13.195 | 14.321 | 11.321 | 0.044 | 12.313 | 7 |
| 1 | 288 | 4 | in1 | 210 | 20.132 | 17.132 | 18.257 | 15.257 | 0.0645 | 18.062 | 7 |
| 1 | 287 | 4 | in1 | 210 | 21.868 | 18.868 | 21.258 | 18.258 | 0.0791 | 22.152 | 7 |
| 1 | 286 | 4 | sg1 | 410 | 23.759 | 20.759 | 22.539 | 19.539 | 0.1824 | 51.074 | 7 |
| 1 | 285 | 4 | sg1 | 410 | 26.26 | 23.26 | 25.04 | 22.04 | 0.2227 | 62.367 | 7 |